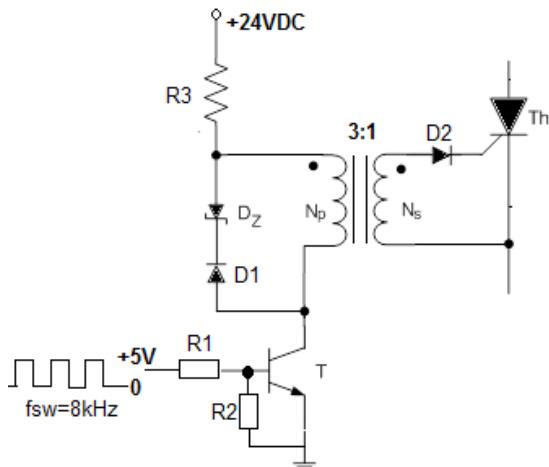


REŠENJE

1.ZADATAK: Monofazni AC/AC pretvarač sa anti-paralelnom spregom služi za regulaciju snage otpornog potrošača koji se napaja iz mreže $380V \pm 15\%$, 50Hz. Na raspolaganju su: tiristorski moduli SKKT460 čiji su podaci dati u Tabeli 1 i hladnjaci serije P16 sa ventilatorom SKF16B čije su karakteristike date u prilogu.

(a) Zahtevana snaga opterećenja je 240kW, maksimalno dozvoljena temperatura silicijuma 110°C , a temperatura okoline se menja u opsegu $-10^{\circ}\text{C} \dots +40^{\circ}\text{C}$. Dimenzionisati sistem hlađenja pretvarača i za tako dimenzionisani sistem odrediti na kojoj maksimalnoj temperaturi se nalazi hladnjak.

(b) Dimenzionisati zaštitno kolo „du/dt“ za tiristore.



(c) Dimenzionisati pobudno kolo tiristora prikazano na slici (R_1 , R_2 , R_3 , V_z), uz pretpostavku da je u kolu gejta tiristora potrebno ostvariti struju od 2A pri naponu gejt-katoda od 3V.

NAPOMENE:

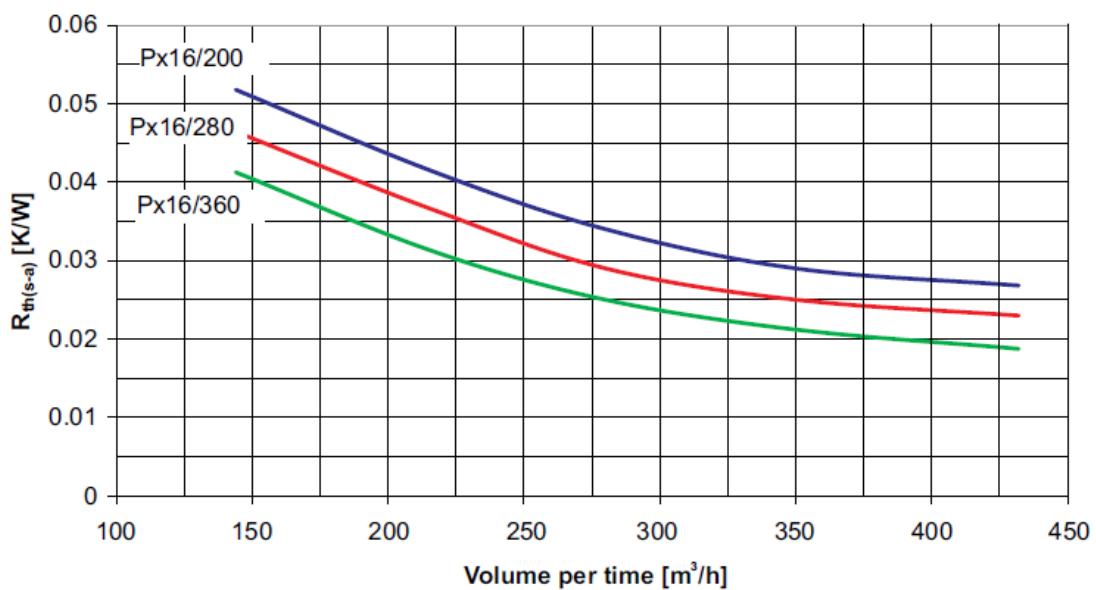
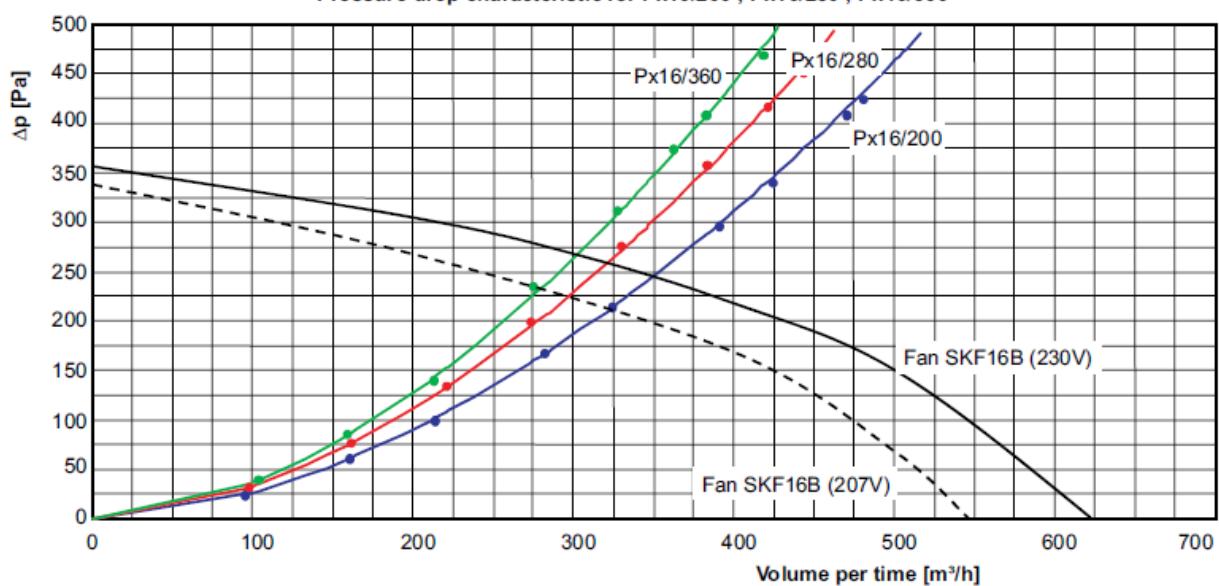
Usvojiti da je pad napona na diodama 0.6V, napon $V_{bes}=0.7\text{V}$, napon $V_{ces}=0.2\text{V}$, pojačanje tranzistora $hfe=350$. Induktivnost magnećenja impulsnog transformatora je 60mH , dok je njegova rasipna induktivnost zanemarljiva.

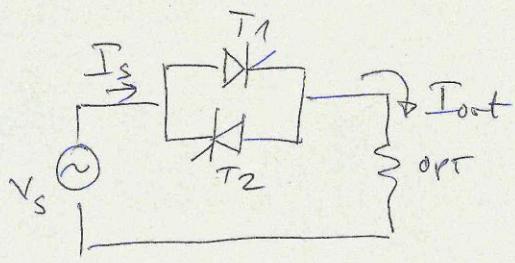
PRILOG ZA ZADATAK 01:

Tabela 1-Karakteristike tiristorskog modula SKKT460

Symbol	Conditions	Values	Units
I_{TAV}	sin. 180; $T_c = 85 (100) ^{\circ}\text{C}$;	460 (335)	A
I_{TSM}	$T_{vj} = 25 ^{\circ}\text{C}; 10 \text{ ms}$	18000	A
	$T_{vj} = 130 ^{\circ}\text{C}; 10 \text{ ms}$	15500	A
i^2t	$T_{vj} = 25 ^{\circ}\text{C}; 8,3 \dots 10 \text{ ms}$	1620000	A^2s
	$T_{vj} = 130 ^{\circ}\text{C}; 8,3 \dots 10 \text{ ms}$	1200000	A^2s
V_T	$T_{vj} = 25 ^{\circ}\text{C}; I_T = 1400 \text{ A}$	max. 1,6	V
$V_{T(TO)}$	$T_{vj} = 130 ^{\circ}\text{C}$	max. 0,88	V
r_T	$T_{vj} = 130 ^{\circ}\text{C}$	max. 0,45	$\text{m}\Omega$
$I_{DD}; I_{RD}$	$T_{vj} = 130 ^{\circ}\text{C}; V_{RD} = V_{RRM}; V_{DD} = V_{DRM}$	max. 240	mA
t_{gd}	$T_{vj} = 25 ^{\circ}\text{C}; I_G = 1 \text{ A}; di_G/dt = 1 \text{ A}/\mu\text{s}$	1	μs
t_{gr}	$V_D = 0,67 * V_{DRM}$	2	μs
$(di/dt)_{cr}$	$T_{vj} = 130 ^{\circ}\text{C}$	max. 250	$\text{A}/\mu\text{s}$
$(dv/dt)_{cr}$	$T_{vj} = 130 ^{\circ}\text{C}$	max. 1000	$\text{V}/\mu\text{s}$
t_q	$T_{vj} = 130 ^{\circ}\text{C} ,$	100 .. 200	μs
I_H	$T_{vj} = 25 ^{\circ}\text{C}; \text{typ. / max.}$	150 / 500	mA
I_L	$T_{vj} = 25 ^{\circ}\text{C}; R_G = 33 \Omega; \text{typ. / max.}$	300 / 2000	mA
V_{GT}	$T_{vj} = 25 ^{\circ}\text{C}; \text{d.c.}$	min. 3	V
I_{GT}	$T_{vj} = 25 ^{\circ}\text{C}; \text{d.c.}$	min. 200	mA
V_{GD}	$T_{vj} = 130 ^{\circ}\text{C}; \text{d.c.}$	max. 0,25	V
I_{GD}	$T_{vj} = 130 ^{\circ}\text{C}; \text{d.c.}$	max. 10	mA
$R_{th(j-c)}$	cont.; per thyristor / per module	0,072 / 0,035	K/W
$R_{th(j-c)}$	sin. 180°; per thyristor / per module	0,074 / 0,037	K/W
$R_{th(j-c)}$	rec. 120°; per thyristor / per module	0,078 / 0,039	K/W
$R_{th(c-s)}$	per thyristor / per module	0,02 / 0,01	K/W
T_{vj}		- 40 ... + 130	$^{\circ}\text{C}$
T_{stg}		- 40 ... + 125	$^{\circ}\text{C}$

Karakteristike hladnjaka i ventilatora
Pressure drop characteristic for Px16/200 ; Px16/280 ; Px16/360





$$V_s = 380 \text{ V} \pm 15\%, 50 \text{ Hz}$$

$$\text{a)} P_{opt} = 240 \text{ kW}$$

Kreditivni snaga je ugodje
najnizi kreznji napon (zec je mba
veća snaga)

$$V_s = 380 - 0,15 \cdot 380 = 323 \text{ V}$$

$$I_{opt} = \frac{P}{V_{smin}} = \frac{240 \text{ kW}}{323 \text{ V}} = 743 \text{ A} \quad (\text{efektivni napon})$$

$$I_{opt} = I_{set} = 743 \text{ A} \quad \text{relativno manji} \quad I_m = \sqrt{2} I_{set}$$

$$I_m = 1047,63 \text{ A}$$

Za svaki od tri stupa V12:

$$I_{T_{1set}} = I_{T_{2set}} = \frac{I_m}{2} = 523,81 \text{ A} \quad (\text{efektivni napon})$$

$$I_{T_{1SR}} = I_{T_{2SR}} = \frac{I_m}{\pi} = \frac{1047,63}{3,14} = 333,64 \text{ A} \quad (\text{red. nivo.})$$

Iz tabele 1 ugovore da je za tri stupnja

$$V_{TO} \approx 0,9 \text{ V} \quad (\text{nivo } i \approx 1 \text{ V}) \quad i \quad r_d = 0,45 \text{ m}\Omega$$

Distribucija snage na emisiju i na trake

$$P_{tot1}^{(1)} = V_{TO} \frac{I_m}{\pi} + r_d I_{set}^2 = V_{TO} \frac{I_m}{\pi} + r_d \left(\frac{I_m}{2}\right)^2$$

$$P_{tot1}^{(1)} = 1 \cdot \frac{1047,63}{\pi} + 0,45 \cdot 10^{-3} \cdot \left(\frac{1047,63}{2}\right)^2$$

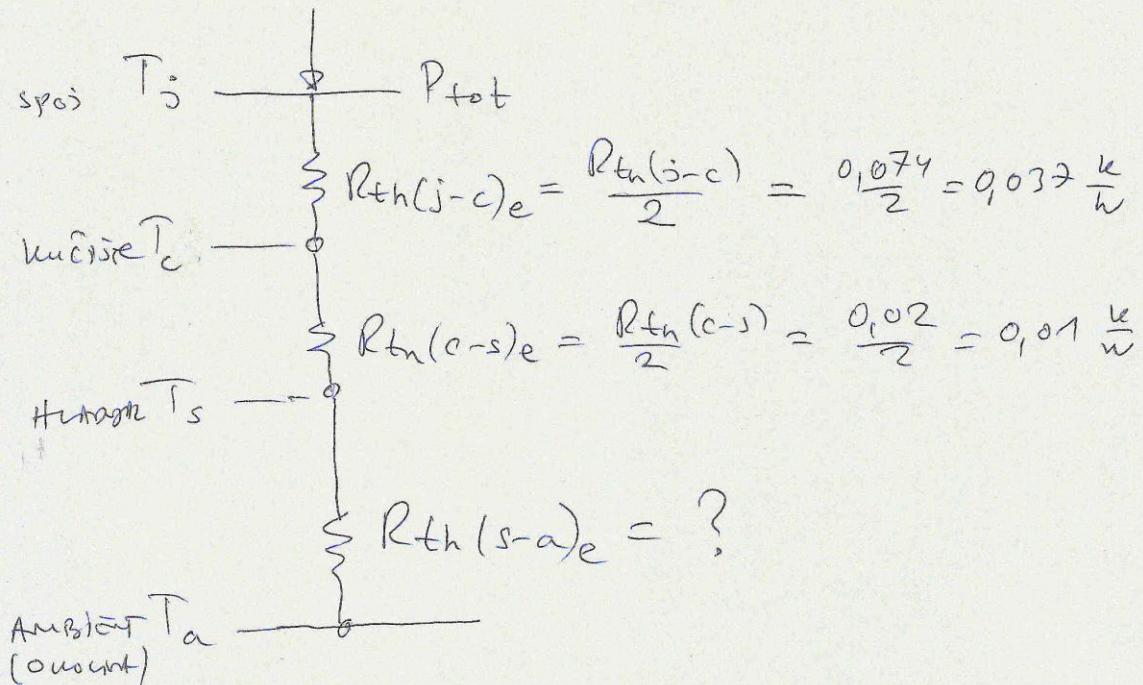
$$P_{tot1}^{(1)} = 333,64 \text{ W} + 123,47 \text{ W} = 457,1 \text{ W}$$

Ukupna snaga distribucije (potrošača) je ugodje
na tri stupnja

$$P_{tot}^{\Sigma} = 2 P_{tot1}^{(1)} = 2 \cdot 457,1 = 914,22 \text{ W}$$

Erläuterung Temperaturschichtung

(2)



$$P_{tot} = \frac{T_j - T_a}{\leq R_{th}} = \frac{T_j - T_a}{R_{th(j-c)} + R_{th(c-s)} + \underbrace{R_{th(s-a)}}_{NEPOZITIV}}$$

$$R_{th(s-a)} = \frac{T_j - T_a}{P_{tot}} - R_{th(j-c)} - R_{th(c-s)}$$

$$R_{th(s-a)} = \frac{110^\circ C - 40^\circ C}{914,22 W} = 0,037 \frac{K}{W} - 0,01 \frac{K}{W}$$

$$R_{th(s-a)} = 0,07657 - 0,037 - 0,01 = 0,0296 \frac{K}{W}$$

$$\text{Oft muss } R_{th(s-a)} \leq 0,0296 \frac{K}{W}$$

SA-Kennzeichnung: $P16/280$ $p_{nr} 300 \text{ m}^3/h$ $p_{nr} 75 \text{ m}$ se

$$R_{th(s-a)}^* = 0,028 \frac{K}{W} \text{ (Gesamt mit Dauerbelastung)}$$

Temperatur Hitzeleistung Ze:

(3)

$$T_s = T_a + P_{tot} \cdot R_{th(s-a)}^*$$

$$T_s = 40^\circ C + 914,22 \text{ W} \cdot 0,028 \frac{\text{K}}{\text{W}} = 65,6^\circ C$$

Temperatur Urelement Ze:

$$T_c = T_s + R_{th(c-s)} \cdot P_{tot} = 65,6^\circ C + 0,01 \cdot 914,22 \frac{\text{K}}{\text{W}} \cdot \text{W}$$

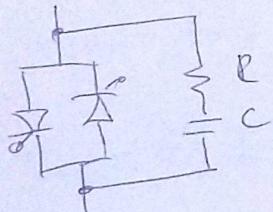
$$T_c = 65,6^\circ C + 9,14^\circ C = 74,74^\circ C$$

Temperatur Si Sp0DA

$$T_j = T_c + R_{th(j-c)} \cdot P_{tot} = 74,74^\circ C + 0,037 \cdot 914,22$$

$$T_j = 108,56^\circ C \leq 110^\circ C$$

b) $\frac{du}{dt}$ Zeigt (RC Zeitkonstante)



$$(\approx 700 \cdot \frac{I_v}{V_v^2}) \text{ MF} \quad * \text{ PREZIVAT}$$

$$V_v = V_{s,eff} + 15\% = 380 \cdot 1,15 = 440 \text{ V}$$

$$I_v = I_{Trans} = I_{Teff} = 523 \text{ A}$$

$$(\approx 700 \cdot \frac{523}{440^2} = 1,89 \text{ MF} \rightarrow 2 \text{ MF})$$

$$R \approx \frac{9000}{C \cdot V_{max}} = \frac{9000}{2 \cdot 440} \approx 10,22 \Omega \quad * \text{ PREZIVAT}$$

Dissipativer Widerstand

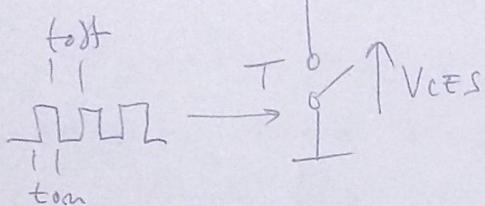
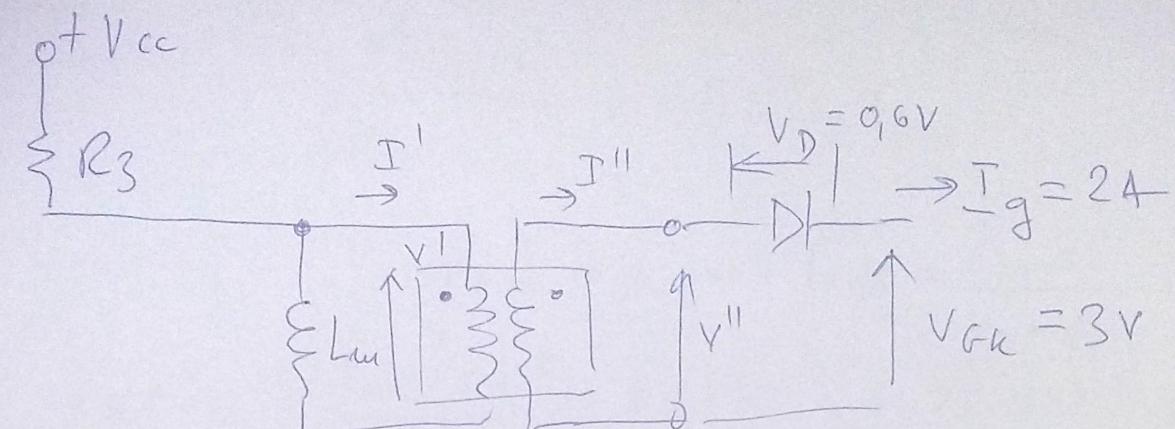
$$P_D \approx 3 \cdot 10^{-6} \cdot C \cdot V_v^2 \cdot f \text{ [W]} \quad * \text{ PREZIVAT} \quad f = 50 \text{ Hz}$$

$$P_D = 3 \cdot 10^{-6} \cdot 2 \cdot 440^2 \cdot 50 = 58 \text{ W}$$

RC Lern
DEFINITION

$$\begin{cases} R = 10 \Omega / 50 \text{ W} \\ C = 2 \text{ MF} / 1000 \text{ V} \end{cases}$$

$$T_N = \frac{1}{f} = \frac{1}{800\text{Hz}} = 125\mu\text{s}$$



$$V'' = V_D + V_{GK}$$

$$V'' = 0.6 + 3 = 3.6V$$

$$V^I = \left(\frac{N^I}{N''}\right) \cdot V'' = 3 \cdot 3.6V = 10.8V \quad I'' = I_g = 2A$$

$$m = 3:1 = 3 \quad I^I = \frac{I''}{m} = \frac{2}{3} =$$

$$t_{on} = t_{off} \quad t_{on} + t_{off} = 125\mu\text{s} \Rightarrow t_{on} = t_{off} = 62.5$$

$$V_{cc} = R_3 I^I + V^I + V_{ces} \Rightarrow R_3 = \frac{V_{cc} - V^I - V_{ces}}{\pm I}$$

$$R_3 = \frac{24 - 10.8 - 0.2}{0.186} = 19.7\Omega \rightarrow 20\Omega$$

$$I_{eff} = \frac{I^I}{\sqrt{2}} = \frac{0.186}{\sqrt{2}} = 0.142A$$

$$P_{R_3} = R_3 I_{eff}^2 = 20 \cdot 0.142^2 = 4.418W \rightarrow 5W$$

$$R_3 = 20\Omega / 5W$$

(5)

$$L_m \cdot \Delta i = V^1 \cdot t_{on} \quad \Delta i = I_m \quad I_m = \frac{V^1 t_{on}}{L_m}$$

$$I_m = \frac{10,8 \cdot 62,5 \mu s}{60 \cdot 10^{-3}} = 11,25 \mu A$$

$$L_m \cdot \Delta i = (V_D + V_Z) \cdot t_{off} \Rightarrow t_{off} = \frac{L_m \cdot \Delta i}{V_D + V_Z} \leq 62,5 \mu s$$

$$V_D + V_Z \geq \frac{L_m \cdot \Delta i}{62,5 \mu s} = \frac{60 \cdot 10^{-3} \cdot 11,25 \cdot 10^{-3}}{62,5 \mu s} = \frac{60 \cdot 11,25 \cdot 10^{-6}}{62,5 \cdot 10^{-6}}$$

$$V_D + V_Z \geq 10,8 V \Rightarrow V_Z \geq 10,8 - 0,6 = 10,2 V$$

~~V max de Zener dioda je~~

$$V_Z = 11 V$$

~~Dioda je zener dioda~~

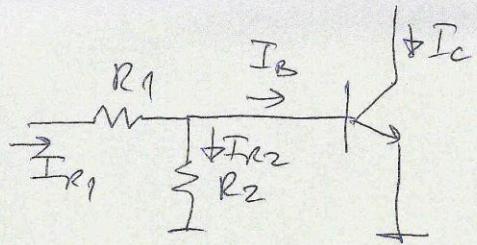
$$P_{DZ} = \frac{V_Z \cdot I_Z}{2} = \frac{V_Z \cdot I_m}{2} = \frac{11 \cdot 11,25 \mu A}{2} = 61,875 \mu W$$

$$V_{max} \text{ je } P_{DZ} = 100 mW$$

Zener dioda uvažme?

$$V_Z^* = 11 V / 100 mW$$

(6)



$$I_{e2} = \frac{V_{BES}}{R_2} = \frac{0,7}{10k} = 0,07 \mu A$$

Umsteigen $R_2 = 10k$

$$I_c = 0,664$$

$$I_B = \frac{I_c}{h_{FE}} = \frac{0,664}{350} = 0,001885 = 1,885 \mu A$$

$$I_{e1} = I_B + I_{e2} = 1,885 \mu A + 0,07 \mu A = 1,955 \mu A$$

$$V_{cc}^{PQB} = R_1 I_{e1} + V_{BES} \Rightarrow R_1 = \frac{V_{cc}^{PQB} - V_{BES}}{I_{e1}} = \frac{5 - 0,7}{2 \mu A}$$

$$R_1 = 2,15 k\Omega \rightarrow \text{mautige } R_1^* = 2 k\Omega$$

$$P_{R1} = R_1 I_{e1}^2 = 2,15 \cdot 10^3 \cdot (2 \mu A)^2 = 8,8 mW$$

$$P_{R2} = R_2 I_{e2}^2 = 10 \cdot 10^3 \cdot (0,07 \mu A)^2 = 0,049 mW$$

Kontrollieren:

$$R_1^* = 2 k\Omega / 10 mW$$

$$R_2^* = 10 k\Omega / 1 mW$$

$$R_3^* = 20 \Omega / 5 W$$