

# VISER-MASTER studije ELIN-PE<sup>2</sup>P 2019/2020

## REŠENJA ZADATAKA-I kolokvijum

### 1. Zadatak

Inteligentni IGBT energetski modul se koristi u AC/AC frekventno regulisanom energetskom pretvaraču. Ulazni mrežni napon je 3x400V, 50Hz. Izgled i osnovne tehničke karakteristike IGBT modula su date u PRILOGU1.

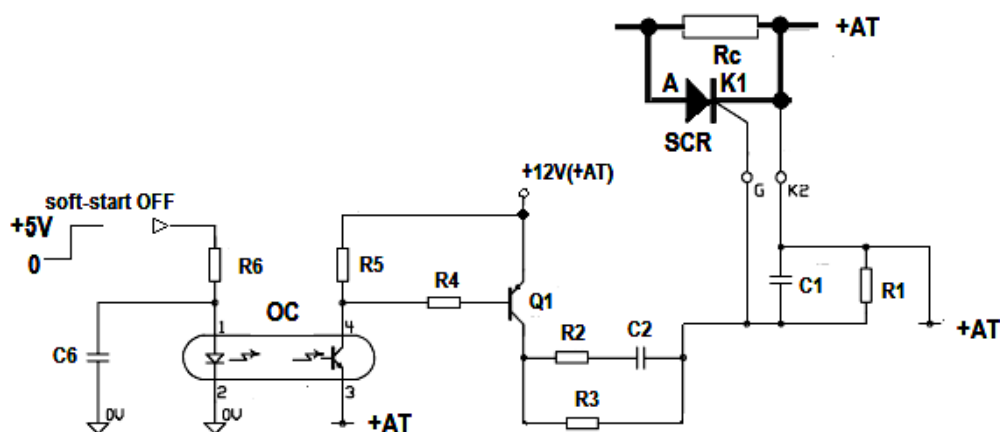
- Nacrtati kompletnu električnu šemu pretvarača: mrežni ulaz-ispravljač-LC filter-kolo za početno punjenje banke elektrolita-kolo za kočenje-izlazni inverter-motor
- Odrediti maksimalnu snagu trofaznog asinhronog motora koji se može priključiti na izlaz modula (tačke 4-5-6)
- Projektovati LC filter u jednosmernom DC međukolu, ako je talasnost DC napona  $<2\%$ , a talasnost DC struje  $<10\%$
- Predložiti i projektovati kolo za početno punjenje banke elektrolita; usvojiti da je maksimalna struja punjenja 30A; Podaci za tiristorski modul su dati u PRILOGU2
- Odabrati tip i projektovati ulazne mrežne osigurače
- Dimenzionisati otpornik za kočenje u DC međukolu

### 2. Zadatak

Za uslove koji su dati u Zadatku 1 odrediti potrebnu termičku otpornost hladnjaka, na koji se montiraju sve poluprovodničke komponente u pretvaraču. Usvojiti da je za ispravljačke elemente  $V_{TO}=1V$ ,  $r_D=5m\Omega$ . Pretpostaviti temperaturni radni opseg  $-25^{\circ}C...+60^{\circ}C$  i maksimalnu temperaturu na poluprovodničkim spojevima od  $T_j=130^{\circ}C$ . Nakon odabira hladnjaka izračunati temperaturu na kućištu modula temperaturu na hladnjaku.

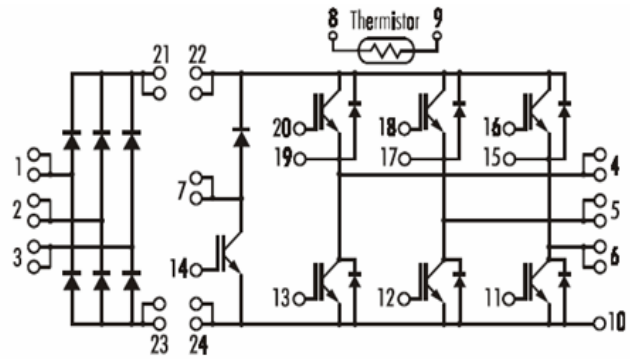
### 3. Zadatak

Dimenzionisati komponente impulsnog pojačavača (Slika 1) za energetski tiristor 100A/1200V- PDT 10012 koji se koristi za početno punjenje elektrolita u Zadatku 1. Pojačanje tranzistora Q1 je  $h_{FE}=40$ ;  $V_{BES}=0.7V$  i  $V_{CES}=0.2V$ . Prenosni odnos optokaplera OC je  $I_C/I_F=10$ . Napon napajanja pojačavača je  $E=12V$ . Ulazni signal je pravougaoni impuls amplitude 5V. Pretpostaviti da forsirano uključenje tiristora traje  $50\mu s$ .



Slika1- pobudno SCR kolo

## PRILOG 1



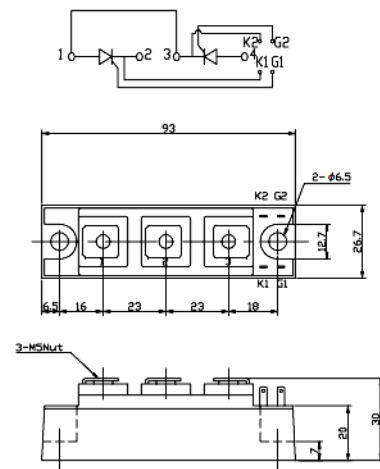
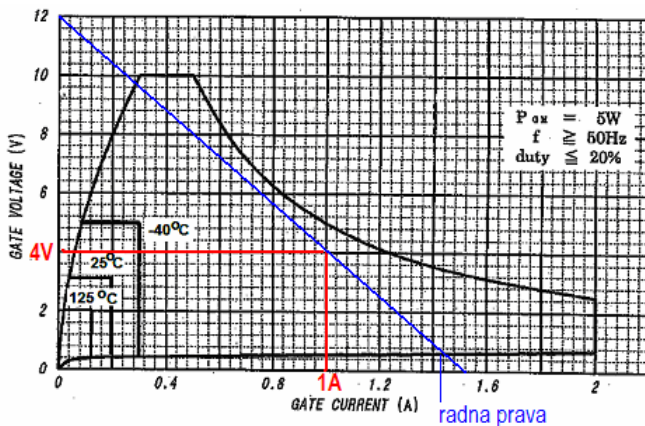
### ■ Absolute Maximum Ratings ( $T_c=25^\circ\text{C}$ )

	Items	Symbols	Test Conditions	Ratings	Units
Inverter	Collector-Emitter Voltage	$V_{CES}$		1200	V
	Gate -Emitter Voltage	$V_{GES}$		$\pm 20$	
	Collector Current	$I_C$	Continuous $25^\circ\text{C} / 80^\circ\text{C}$	75 / 50	A
		$I_{C\text{ PULSE}}$	1ms $25^\circ\text{C} / 80^\circ\text{C}$	150 / 100	
		$-I_{C\text{ PULSE}}$		50	
	Collector Power Dissipation	$P_C$	1 device	360	W
Rectifier	Repetitive Peak Reverse Voltage	$V_{RRM}$		1600	V
	Average Output Current	$I_O$	50Hz/60Hz sinus wave	50	A
	Surge Current (Non Repetitive)	$I_{FSM}$	$T_J=150^\circ\text{C}$ , 10 ms, sinus wave	520	
	$I^2t$ (Non Repetitive)			1352	$\text{A}^2\text{s}$
Brake Chopper	Collector-Emitter Voltage	$V_{CES}$		1200	V
	Gate -Emitter Voltage	$V_{GES}$		$\pm 20$	
	Collector Current	$I_C$	Continuous $25^\circ\text{C} / 80^\circ\text{C}$	35 / 25	A
		$I_{C\text{ PULSE}}$	1ms $25^\circ\text{C} / 80^\circ\text{C}$	70 / 50	
	Collector Power Dissipation	$P_C$	1 device	180	W
	Repetitive Peak Reverse Voltage	$V_{RRM}$		1200	V
	Operating Junction Temperature	$T_J$		+150	$^\circ\text{C}$
	Storage Temperature	$T_{Stg}$		-40 ~ +125	
	Isolation Voltage	$V_{ISO}$	A.C. 1min.	2500	V
	Mounting Screw Torque*			3.5	Nm

### ■ Thermal Characteristics

Items	Symbols	Test Conditions	Min.	Typ.	Max.	Units
Thermal Resistance (1 device)	$R_{\theta(j-c)}$	Inverter IGBT			0.35	$^\circ\text{C/W}$
		Inverter FRD			0.75	
		Brake IGBT			0.69	
		Rectifier Diode			0.50	
		With Thermal Compound		0.05		
Contact Thermal Resistance	$R_{\theta(c-s)}$	With Thermal Compound		0.05		

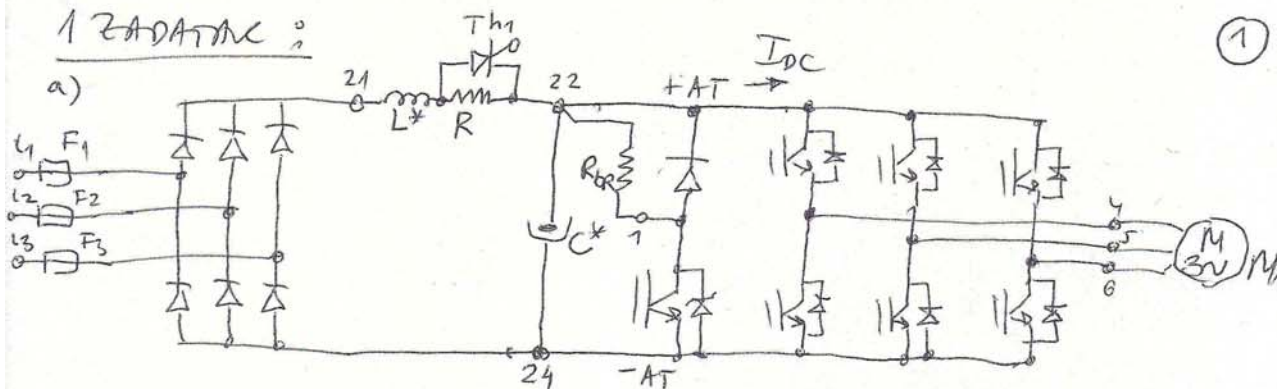
## PRILOG 2



**Tehnički podaci:**  $V_{DRM}=1200\text{V}$ ,  $I_{OAVG}=100\text{A}$ ,  $I_{ORMS}=150\text{A}$ ;  $I_{GT}=200\text{mA}$ ,  $V_{GT}=4\text{V}$ ;  $R_{\theta(j-c)}=0.35\text{K/W}$ ,  $R_{\theta(c-s)}=0.2\text{K/W}$

# 1 ZADATAK :

1



- b) IZLAZNA SNAGA IGBT INVERTERA JE  $I_c = 50A$  (KONTINUALNA SNAGA) NA  $80^\circ C$

$$2P_{\text{MOT}} [\text{kW}] \approx I_c [A], \text{ odnosno } P_{\text{MOT}}^{\text{max}} \approx \frac{50}{2} = 25 \text{ kW}$$

USVOJIMO DA JE NA IZLAZU INVERTERA PROJEKTOVAN FUNKCIONISANJE MOTORA  $M_1$  22 kW; 400V, 50Hz;  $\eta = 0.92$ ;  $\cos \varphi = 0.85$

$$P_{\text{ee}}^{\text{MOT}} = \frac{P_{\text{MOT}}}{\eta} = \frac{22 \text{ kW}}{0.92} = 23.9 \text{ kW}$$

$$I_{\text{MOT}} = \frac{P_{\text{ee}}^{\text{MOT}}}{\sqrt{3}U \cdot \cos \varphi} = \frac{23.9 \text{ kW}}{\sqrt{3} \cdot 0.4 \text{ kV} \cdot 0.85} = 41.4 < 50 A$$

- c) NAPON DC MEĐU-KOLA

$$U_{\text{DC}} = \frac{3V_m}{\pi} \quad V_m = 400\sqrt{2} \quad U_{\text{DC}} = \frac{3 \cdot 400\sqrt{2}}{\pi} = 538.8 \text{ V}^*$$

\* ZAMETANJE DA PISANJE NAPONA NA BODU A U ISTR. MOTA.

$$P_{\text{DC}} = U_{\text{DC}} I_{\text{DC}} \quad P_{\text{DC}} \cdot \eta_{\text{inv}} = P_{\text{ee}}^{\text{MOT}} \Rightarrow P_{\text{DC}} = \frac{P_{\text{ee}}^{\text{MOT}}}{\eta_{\text{inv}}} = P_{\text{ee}}^{\text{MOT}} + P_{\text{fe}}^{\text{inv}}$$

NA OSNOVU TABELE U PRILOGU 1 OBRISI U INVERTERU DA

$$P_{\text{fe}}^{\text{inv}} \approx 360 \text{ W}, \text{ USVOJIMO } P_{\text{fe}}^{\text{inv}} = 400 \text{ W}$$

$$P_{\text{DC}} = P_{\text{ee}}^{\text{MOT}} + P_{\text{fe}}^{\text{inv}} = 23.9 \text{ kW} + 0.4 \text{ kW} = 24.3 \text{ kW}$$

$$I_{\text{DC}} = \frac{24.3 \text{ kW}}{538.8 \text{ V}} = 45.1 A$$

(2)

$$\delta_{n_i} \leq 2\% \quad \delta_{i_i} \leq 10\%$$

избор конденз. C

$$C \geq \frac{1}{n \cdot \omega \cdot R_{\text{отенр}}} \cdot \frac{\delta_{i_i}}{\delta_{n_i}}$$

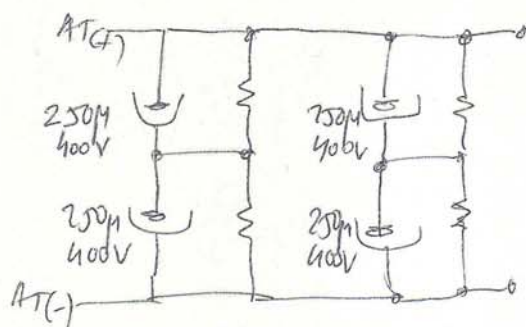
$$n = 6 \text{ (6 пульси 13 прамито)}$$

$$\omega = 2\pi f = 2\pi \cdot 50 \text{ Hz} = 314 \text{ rad/s}$$

$$R_{\text{отенр}} = \frac{U_{DC}}{I_{OC}} = \frac{538,8}{45,1} = 11,95 \Omega$$

$$C \geq \frac{1}{6 \cdot 314 \cdot 11,95} \cdot \frac{10}{2} = 222 \mu\text{F} \xrightarrow{\text{на база}} C^* = 250 \mu\text{F}/400\text{V}$$

БАЗЕЈНА БАКА

НАПОМЕНА:  
МОЗЕ СЕ ИСВОДИи кондензоре  $C^* = 330 \mu\text{F}/400\text{V}$ 

$$\text{критична индуктност } L_{kr} = \frac{R_{\text{отенр}}}{105\omega} = \frac{11,95}{105 \cdot 314} = 0,36 \text{ mH}$$

Индуктност L:

$$L \geq \frac{1}{(6\omega)^2 C^*} \cdot \frac{4 R_{\text{отенр}} \cdot 6\omega C^*}{35 \cdot \delta_{i_i}} + \frac{1}{(6\omega)^2 C^*}$$

$$\delta_{i_i} = \frac{\delta_{i_i} \%}{100} = \frac{10}{100} = 0,1$$

$$L \geq \frac{4 \cdot R_{\text{отенр}}}{35 \cdot 6\omega \cdot \delta_{i_i}} + \frac{1}{(6\omega)^2 C^*}$$

$$L \geq \frac{4 \cdot 11,95}{35 \cdot 6 \cdot 314 \cdot 0,1} + \frac{1}{(6 \cdot 314)^2 \cdot 250\mu}$$

$$L \geq 7,25 \text{ mH} + 1,12 \text{ mH} = 8,37 \text{ mH} \xrightarrow{\text{на база}} L^* = 8,5 \text{ mH}/50\text{A}$$



(3)

$$I_{DC} = 45,1A \quad \Delta I_{DC} = 0,1 I_{DC} = 0,1 \cdot 45,1 = 4,51A$$

$$I_{Lmax} = 45,1 + \frac{4,51}{2} = 47,4A \rightarrow \text{usvajamo } I_{Lmax} = 50A$$

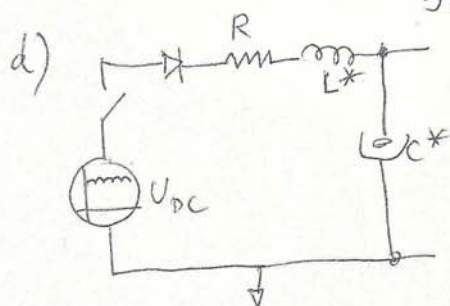
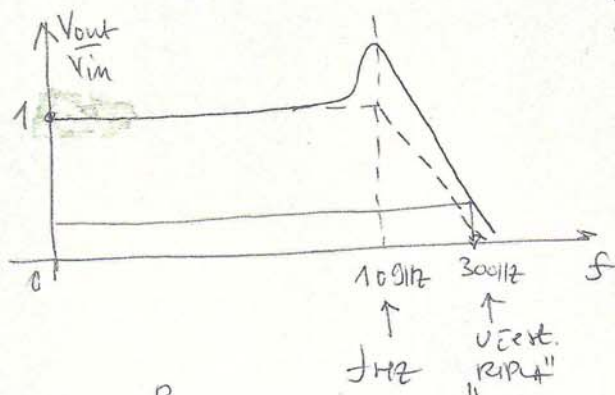
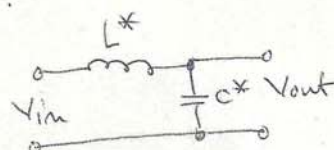
$$L^* = 8,5mH / 50A$$

REZONANCA UČESTANOST "LC" FILTRA

$$\omega_{rez} = \frac{1}{\sqrt{L^* C^*}} = \frac{1}{\sqrt{8,5m \cdot 0,75m}} = 686 \text{ rad/s}$$

$$f_{rez} = \frac{\omega_{rez}}{2\pi} = \frac{686}{6,28} = 109,21Hz$$

PREVOZNA F-NA "LC" FILTRA



Bez otpornika R MAX snaga  
prijemnika kondenzator C je:

$$I_{Cmax} = \frac{U_{DC}}{Z_C} = \frac{U_{DC}}{\sqrt{\frac{L^*}{C^*}}} = \frac{538,8}{\sqrt{\frac{8,5m}{0,75m}}}$$

$$I_{Cmax} = \frac{538,8}{5,83} \approx 92,4A \approx 93A$$

Otpornik R se bira tako da zadovolji kritičan otpor  $R_{kr} = 2\sqrt{\frac{L^*}{C^*}}$

$$R_{kr} = 11,66\Omega \quad \text{usvajamo } R = 12\Omega$$

$$\text{Snaga max. snaga prijemnika } I_{Cmax}' = \frac{1,1 U_{DC}}{R + Z_C} = \frac{1,1 \cdot 538,8}{12 + 5,83}$$

$$I_{Cmax}' = \frac{593}{17,83} = 33,26A$$

ZA OGRANIČENJE snage prijemnika od 30A, treba izbora

$$I_{Cmax}'' = 30A \quad \frac{1,1 U_{DC}}{R + Z_C} = 30 \quad R + Z_C = \frac{1,1 U_{DC}}{30} \Rightarrow R = \frac{1,1 U_{DC}}{30} - Z_C = 14\Omega$$

usvajamo  $R = 14\Omega / 100W$

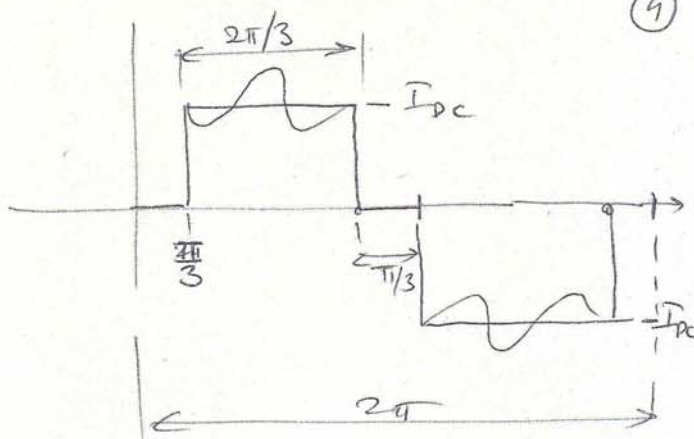
e)  $I_{DC} = 45,1 \text{ A}$

Efektivna vrednost  
ulazne struje

$$I_{Leff} = \sqrt{\frac{2 I_{DC}^2 \cdot \frac{2\pi}{3}}{2\pi}}$$

$$I_{Leff} = \sqrt{\frac{2}{3}} I_{DC}$$

$$I_{Leff} = \sqrt{\frac{2}{3}} \cdot 45,1 = 36,8 \text{ A}$$



- Maksimalna struja je 40A, napona 650V
- Ograničenje po brzini ulaza (VBO)

$$I^2 t(\text{otvoreno}) \geq I^2 t(\text{VBO})$$

Pretpostavimo  $I^2 t(\text{otvoreno}) \approx 2 I^2 t(\text{VBO})$

$$\Rightarrow I^2 t(\text{VBO}) = \frac{1}{2} I^2 t(\text{otvoreno}) = \frac{1}{2} \cdot 1352 \text{ A}^2 \cdot \text{s}$$

$$I^2 t(\text{VBO}) \approx 670 \text{ A}^2 \cdot \text{s}$$

VBO:

$$40 \text{ A} / 650 \text{ V} ; 670 \text{ A}^2 \cdot \text{s}$$

f)  $P_{BR} \approx 1,2 \frac{U_{DC}^2}{R_{BR}} \quad P_{BR} \approx P_{mot}^{el} = 23,9 \text{ kW}$

$$R_{BR} = \frac{1,2 U_{DC}^2}{P_{BR}} = \frac{1,2 \cdot 538,8^2}{23,9 \text{ kW}} = 14,57 \Omega \rightarrow 15 \Omega$$

$$R_{BR} = 15 \Omega / 1 \text{ kW cont.} \quad t_u \approx 1 \text{ s} \quad E = \frac{1,2 \cdot 538,8^2}{15 \Omega} \cdot 1 \text{ s} = 6,45 \text{ kWh}$$

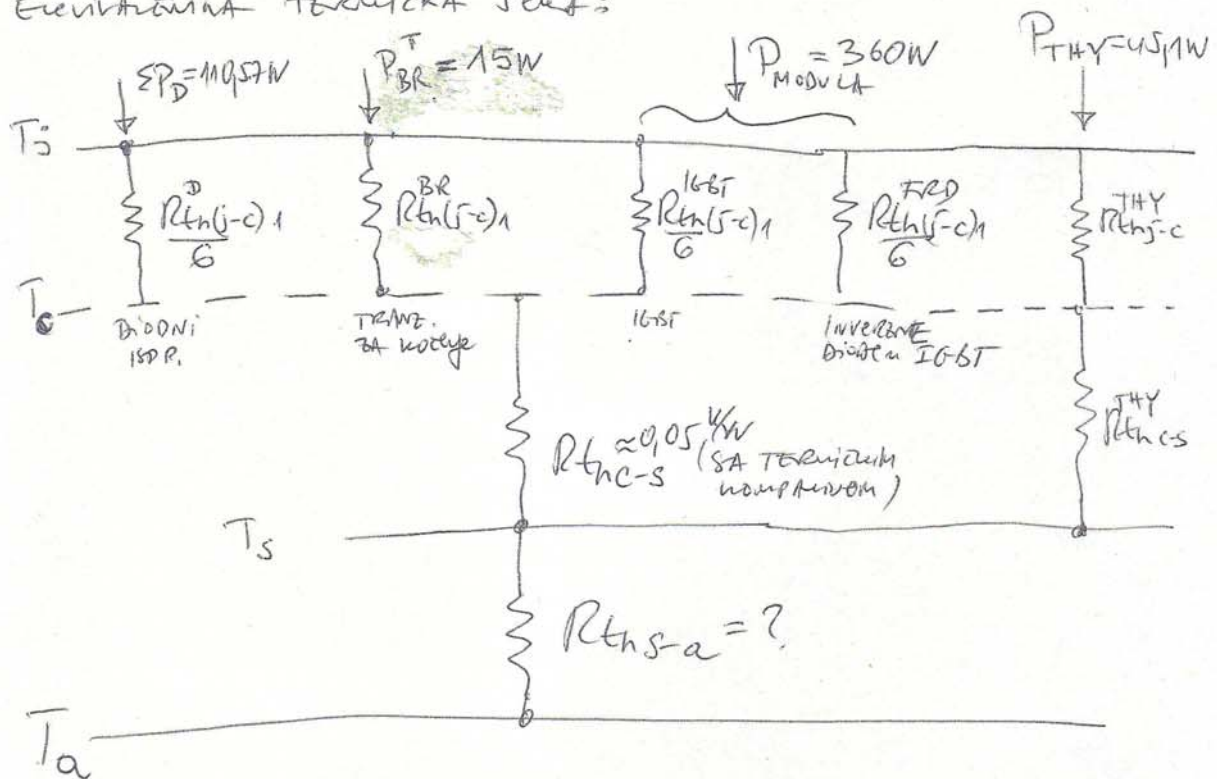
## 2 ZADANJE

(5)

$$V_{TO} = 1V \quad r_d = 5m\Omega$$

$$-25^\circ C \dots +60^\circ C \quad T_{jmax} = 130^\circ C$$

EVOLUCIJA TEHNIKA JENI:



\*  $\Sigma P_D = 6 \cdot P_{D1}$  - disipacija na diodama istaknutih

$$P_{D1} = V_{TO} I_{Dsr} + r_d \cdot I_{Deff}^2 \quad I_{Dsr} = \frac{I_{DC}}{3} = \frac{45.1}{3} = 15.03A$$

$$P_{D1} = 1 \cdot 15.03 + 5 \cdot 10^{-3} \cdot 76.07^2 \quad I_{Deff} = \frac{I_{DC}}{\sqrt{3}} = \frac{45.1}{\sqrt{3}} = 26.07A$$

$$P_{D1} = 18.42W$$

$$P_D = 6P_{D1} = 110.57W$$

\*  $P_{BR}^T \approx 60W \left( \frac{1}{6} \cdot 360W \right) \rightarrow$  OBRATNO DA SE KOTIRNI OPORENI NE MNYAJE ČESTO MORENO MNYAJE

$$P_{BR}^T \approx 10 \div 20W \text{ (maksimum 15W)}$$

$$* P_{MODULA} = 360W$$



\*  $P_{THY} = V_{TO} \cdot I_{DC} = 1.45,1 \approx 45,1 \text{ W}$

(6)

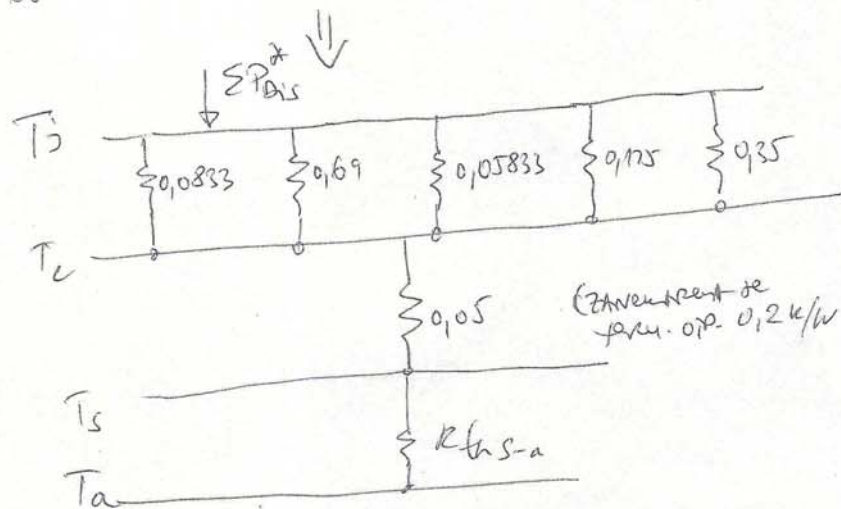
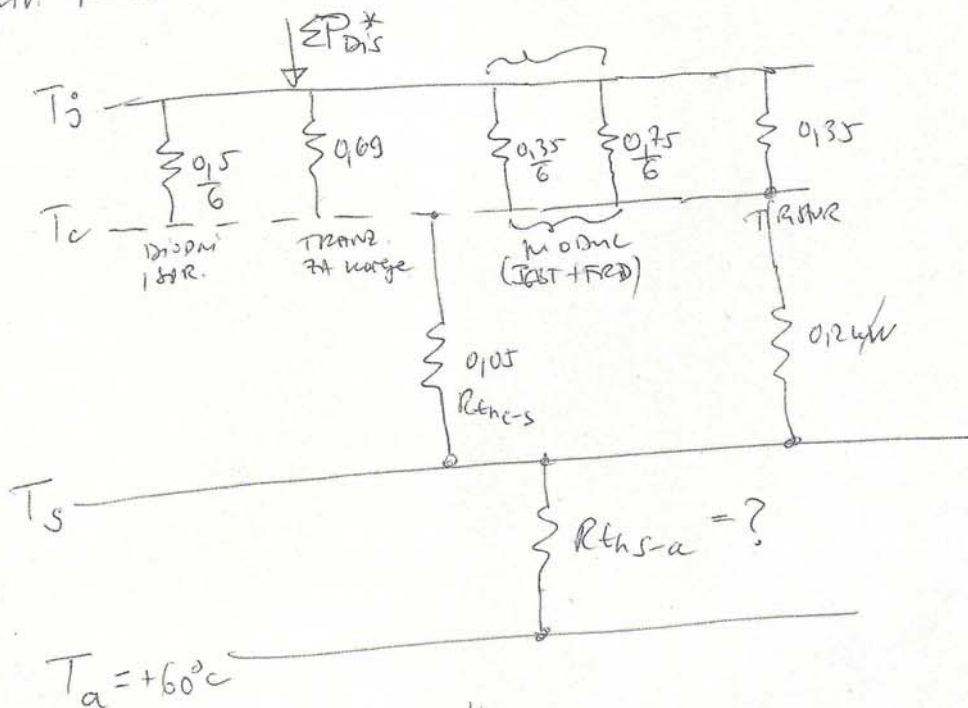
Umarul sursa distribuite sunt echivalat la temperatură de

$$\begin{aligned} \sum P_{Dis} &= \sum P_D + P_{BR}^T + P_{modula} + P_{THY} \\ &= 110,57 \text{ W} + 15 \text{ W} + 360 \text{ W} + 45,1 \text{ W} = 530,67 \text{ W} \end{aligned}$$

Presupunem ca se realizează o distribuție a surselor de

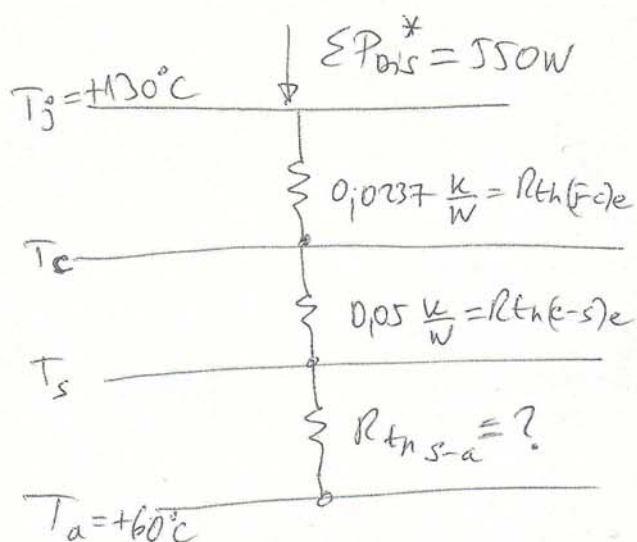
$$\sum P_{Dis}^* = 550 \text{ W}$$

Ecuv. rezolvată este de :





(7)



$$R_{th(s-a)} + R_{th(j-c)} + R_{th(c-s)} \leq R_{th}^*$$

$$R_{th}^* = \frac{T_{jmax} - T_{amax}}{\Sigma P_{dis}^*}$$

$$R_{th(s-a)} + R_{th(j-c)} + R_{th(c-s)} \leq \frac{T_{jmax} - T_{amax}}{\Sigma P_{dis}^*}$$

$$R_{th(s-a)} + 0.0237 + 0.05 \leq \frac{130^\circ - 60^\circ}{550\text{W}}$$

$$R_{th(s-a)} \leq \frac{130-60}{550} - 0.0237 - 0.05$$

$$R_{th(s-a)} \leq 0.127 - 0.0237 - 0.05 = 0.0535 \frac{\text{K}}{\text{W}} \left( \frac{^\circ\text{C}}{\text{W}} \right)$$

$$\text{Usvoricenost } R_{th(s-a)}^* = 0.05 \frac{\text{K}}{\text{W}}$$

— TEMPERATURA NA HLAVNICI NA OVIH MASTIMA VNEŠNOST JE:

$$T_s = T_a + R_{th(s-a)} \cdot \Sigma P_{dis}^* = 60^\circ\text{C} + 0.05 \cdot 550 = 87.5^\circ\text{C}$$

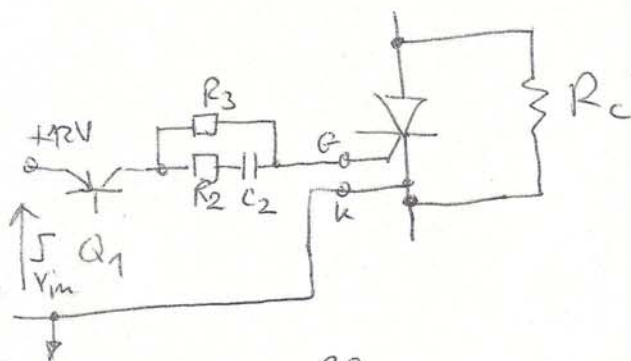
— TEMPERATURA NA KUCIJM MODULA

$$T_c = T_s + R_{th(c-s)} \cdot \Sigma P_{dis}^* = 87.5^\circ\text{C} + 0.05 \cdot 550$$

$$T_c = 115^\circ\text{C}$$

### 3 ZADATOK

(8)



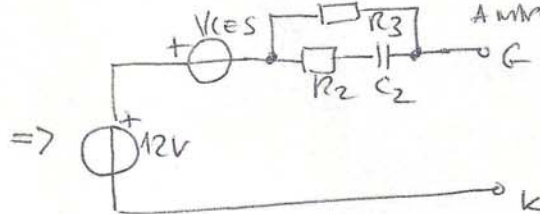
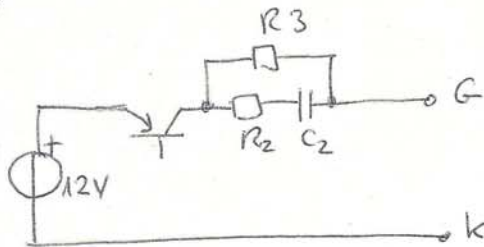
$$V_{BE} = 0.7V$$

$$V_{CE} = 0.2V$$

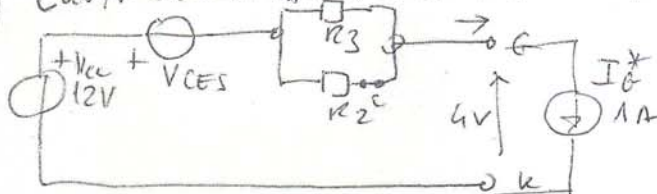
$$h_{FE} = 40$$

$$I_D/I_F = 60$$

NA OSNOVE DIZAJNA 12  
PRILOGA 2 UPOVREDO DA JE  
FUNKCIONALNA GRADIVA GOSTA  $I_G^* = 1A$   
AMBA  $V_{GK} = 4V$



A) EKVIV. JENI ZA FUNKCIONALNI NIZI (NA OSNOVI IZVOR. NOD. 2E, 4S")



$$V_{CC} = V_{CE} + (R_3 \parallel R_2) I_G^* + V_{GK}$$

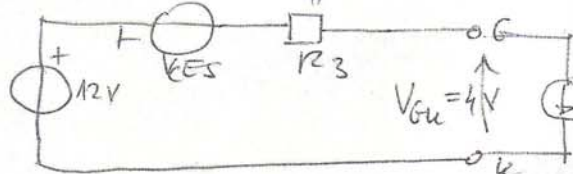
$$I_G^* = \frac{V_{CC} - V_{CE} - V_{GK}}{R_2 \parallel R_3}$$

$$I_G^* = \frac{V_{CC} - V_{CE} - V_{GK}}{\frac{R_2 R_3}{R_2 + R_3}}$$

$$\frac{R_2 R_3}{R_2 + R_3} = \frac{V_{CC} - V_{CE} - V_{GK}}{I_G^*} = \frac{12V - 0.2V - 4V}{1A} = 7.8\Omega$$

$$\boxed{\frac{R_2 R_3}{R_2 + R_3} = 7.8\Omega}$$

B) EKVIV. JENI ZA "UPOVREDO REZILI"



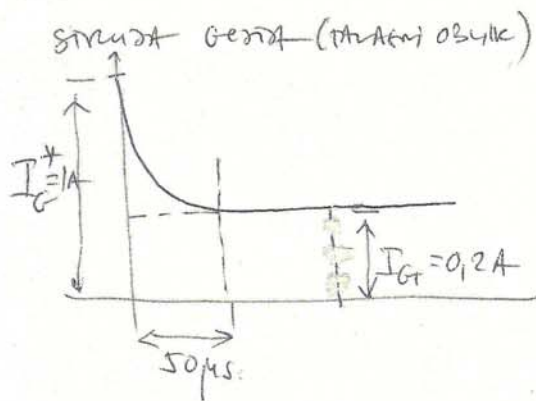
$$R_3 = \frac{V_{CC} - V_{CE} - V_{GK}}{I_{GT}}$$

$$R_3 = \frac{12 - 0.2 - 4}{0.2} = 39\Omega$$

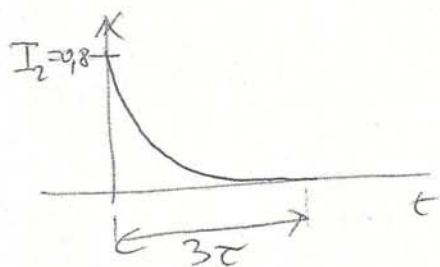
$$R_3 = 39\Omega$$

$$\frac{1}{R_2} + \frac{1}{R_3} = \frac{1}{7.8} \Rightarrow \frac{1}{R_2} = \frac{1}{7.8} - \frac{1}{39} = 0.128 - 0.0256 = 0.1023$$

$$R_2 = 9.76 \rightarrow R_2 = 10\Omega$$



$$I_2 = 1A - 0.2 = 0.8A$$



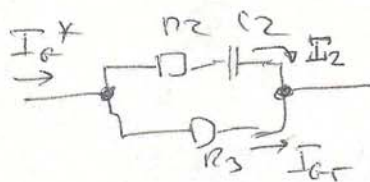
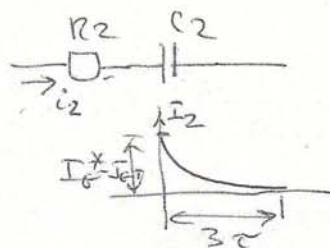
Distribusi  $R_2$ :

$$P_{R2} = R_2 I_2^2 = 10 \cdot 0.8^2 = 6.4W$$

$$P_{R2} = 6.4W \text{ (in transient } \infty 50\mu s)$$

Distribusi  $R_3$ :

$$P_{R3} = R_3 I_{R3}^2 = 30 \cdot 0.2^2 = 1.2W$$



$$I_2 + I_{GT} = I_G^*$$

$$i_2 = I_2 e^{-\frac{t}{\tau}}$$

$$3\tau = 50\mu s$$

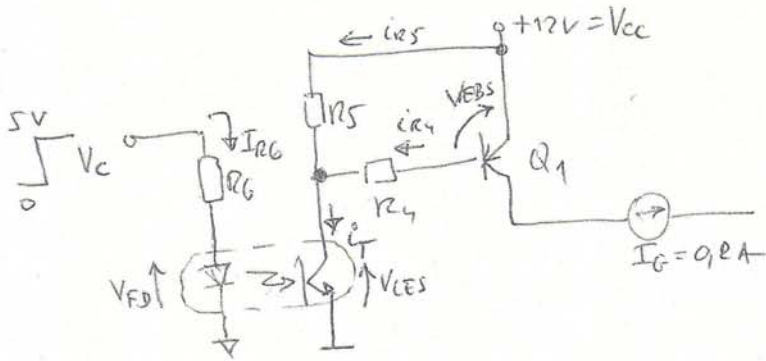
$$3 \cdot R_2 C_2 = 50\mu s \quad R_2 C_2 = \frac{50}{3} \mu s$$

$$C_2 = \frac{50}{3} \mu s \cdot \frac{1}{R_2} = \frac{50}{3} \cdot \frac{1}{10} \mu F = 1.66 \mu F$$

$$C_2^* = 2.2 \mu F$$

\* ПРОБЛЕМЫ ОПОРНЫХ  $R_4, R_5, R_6$

(10)



$$V_c = R_6 I_{R6} + V_{FD}$$

$V_{FD}$  - НАПРЯЖЕНИЕ НА ДИОДЕ  
ОПОРНОГО

$$V_{FD} = 1,2V$$

$$V_c = 5V \quad V_{FD} = 1,2V$$

$$I_{R6} = 2 \mu A \text{ (уставлено)}$$

$$R_6 = \frac{V_c - V_{FD}}{I_{R6}} = \frac{5 - 1,2}{2 \mu} = 1,9k$$

$$R_6^* = 2k / 0,25W$$

ОПНОС ОС

$$\frac{I_T}{I_F} = \left( \frac{I_C}{I_F} \right) \cdot I_{R6}$$

$$I_T = 10 \cdot 2 \mu A = 20 \mu A$$

$$I_{R4} = \frac{I_C}{h_{FE}} = \frac{I_G}{h_{FE}} = \frac{0,2}{40} = 5 \mu A$$

$$V_{CC} = V_{EBS} + R_4 I_{R4} + V_{CES}$$

$$V_{CC} = \underbrace{V_{EBS}}_{0,7V} + R_4 I_{R4} + 0,2V$$

$$\frac{12 - 0,7 - 0,2}{I_{R4}} = R_4$$

$$\frac{11,1}{5 \mu} = R_4 \Rightarrow \frac{11,1}{5 \mu} = 2k2$$

$$R_4 = 2k2 \quad P_{R4} = 2k2 (5 \mu)^2 = 0,055W$$

$$R_4^* = 2k2 / 0,25W$$

$$V_{CC} = R_5 I_{R5} + V_{CES}$$

$$\frac{V_{CC} - V_{CES}}{I_{R5}} = R_5$$

$$R_5 = \frac{12 - 0,2}{15 \mu} = 786,72$$

настройка

$$R_5^* = 1k / 0,25W$$