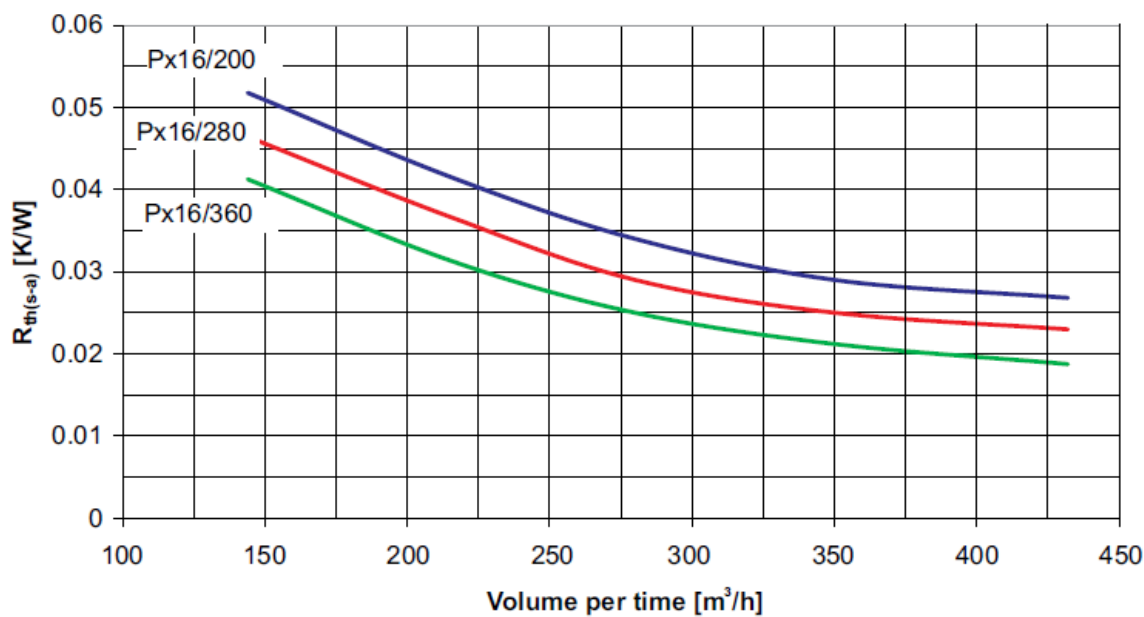
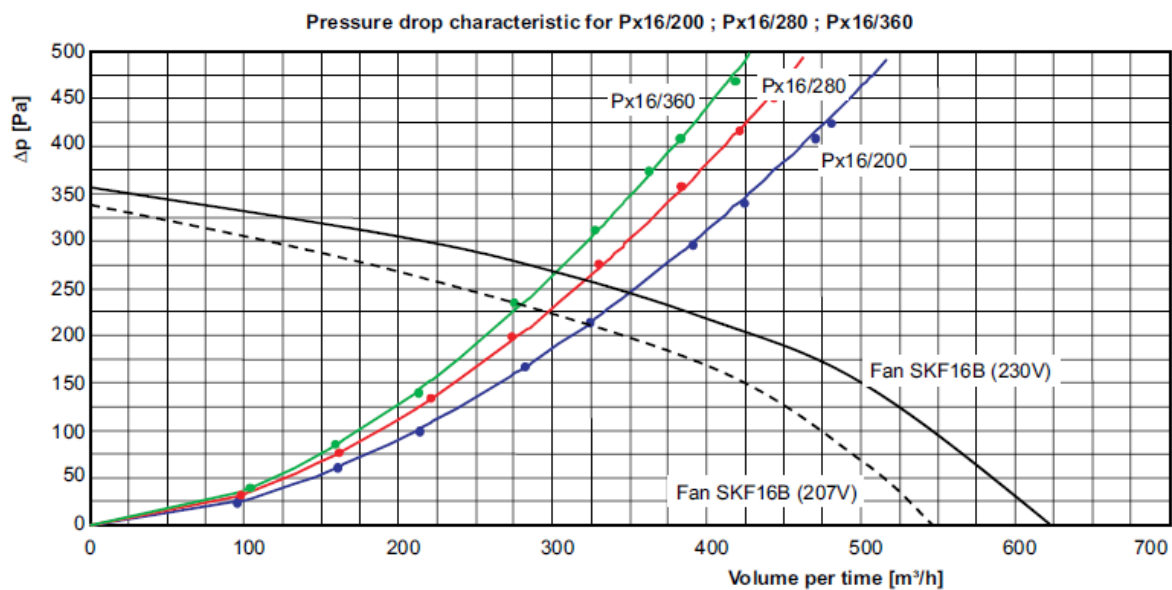


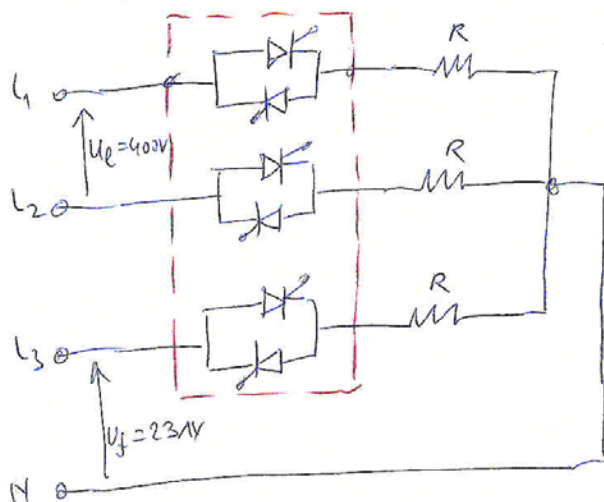


# PRILOG: Karakteristike hladnjaka i ventilatora



REŠENJE:

(1)



$$T_{jmax} = 110^{\circ}\text{C}$$

$$T_a = -10^{\circ}\text{C} \dots + 40^{\circ}\text{C}$$

$$T_j - T_a = P_{tot} \cdot (\sum R_{th})$$

$$P_{tot} = \frac{T_j - T_a}{R_{thj-c} + R_{thc-s} + R_{thsa}}$$

IZ TABELE 1:

$$R_{thj-c} = 0,074 \text{ K/W}$$

$$R_{thc-s} = 0,02 \text{ K/W}$$

$$P_{tot1} \text{ pri } T_{a1} = -10^{\circ}\text{C}$$

$$P_{tot2} \text{ pri } T_{a2} = +40^{\circ}\text{C}$$

$$P_{tot1} = \frac{T_j - T_{a1}}{R_{th(j-c)} + R_{th(c-s)} + R_{th(s-a)}}$$

$$R_{th(j-c)} = \frac{0,074}{6} = 0,01233 \text{ K/W}$$

$$R_{th(c-s)} = \frac{0,02}{6} = 0,00333 \text{ K/W}$$

$$R_{th(s-a)} = 0,025 \text{ K/W}$$

ZA PROJEKTOVANJE 280 m<sup>3</sup>/h IZ

HYDRAULIC P16/360

\* VZROK NA VENTILATOR RANJ

PRI NAJVEĆOJ ROKOVANOSTI 207 V

$$P_{tot1} = \frac{110^{\circ}\text{C} - (-10^{\circ}\text{C})}{(0,01233 + 0,00333 + 0,025) \frac{\text{K}}{\text{W}}} = \frac{120^{\circ}\text{C}}{0,04066 \frac{\text{K}}{\text{W}}} = 2951,3 \text{ W}$$

$$P_{tot2} = \frac{110^{\circ}\text{C} - 40^{\circ}\text{C}}{0,04066 \frac{\text{K}}{\text{W}}} = 1721,6 \text{ W}$$

$$P_{tot1}^{(1)} = V_{TO} \cdot \frac{I_{m1}}{\pi} + r_d \cdot \frac{I_{m1}^2}{4}$$

$$I_{Tse} = \frac{I_{m1}}{\pi} \quad I_{Teff} = \frac{I_{m1}}{2}$$

SMATRA OBLASTI PO DEONICI  
DIZAJNERA

$$P_{tot1}^{(1)} = \frac{P_{tot1}}{6} = 491,88 \text{ W}$$

$$P_{tot1}^{(1)} = V_{T0} \cdot \frac{I_{m1}}{\pi} + r_d \frac{I_{m1}^2}{4} \quad / \cdot \frac{4}{r_d}$$

(2)

$$\frac{4}{r_d} \cdot P_{tot1}^{(1)} = \frac{4V_{T0}}{\pi r_d} I_{m1} + I_{m1}^2 \Rightarrow I_{m1}^2 + \frac{4V_{T0}}{\pi r_d} I_{m1} - \frac{4}{r_d} P_{tot1}^{(1)} = 0$$

$$I_{m1} = \frac{-\frac{4V_{T0}}{\pi r_d} \pm \sqrt{\left(\frac{4V_{T0}}{\pi r_d}\right)^2 - 4 \cdot \left(-\frac{4}{r_d} P_{tot1}^{(1)}\right)}}{2}$$

$$ax^2 + bx + c = 0$$

$$x_{1/2} = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

$$I_{m1} = -\frac{2V_{T0}}{\pi r_d} \pm \sqrt{\frac{4V_{T0}^2}{(\pi r_d)^2} + \frac{16P_{tot1}^{(1)}}{4r_d}}$$

$$a = 1$$

$$b = \frac{4V_{T0}}{\pi r_d}$$

$$c = -\frac{4}{r_d} P_{tot1}^{(1)}$$

IZ TABELE 1:

$$V_{T0} = 0,9V \quad r_d = 0,45m\Omega$$

$$P_{tot1}^{(1)} = 491,88W$$

$$I_{m1} = -\frac{2 \cdot 0,9 \cdot 10^3}{\pi \cdot 0,45} \pm \sqrt{\frac{4 \cdot (0,9)^2}{(\pi \cdot 0,45)^2} \cdot 10^6 + \frac{16 \cdot 491,88}{4 \cdot 0,45} \cdot 10^3}$$

$$I_{m1} = -1273,88 + \sqrt{1622783,88 + 4372266,668}$$

$$I_{m1} = -1273,88 + 2448,48 = 1174,6A$$

EFECTIVA MEDNOST GRUBE OPERACIJA USTANOVE USTRE  
OSTANIOI JE

$$I_{eff_{gr1}} = \frac{I_{m1}}{\sqrt{2}} = 833A$$

PREVODNA BRATA PRI OBLI USKUPET JE  $S_{opt} = 3 \cdot U_f \cdot I_f$

$$S_{opt1} = 3 \cdot \frac{400V}{\sqrt{3}} \cdot 833A = 577,83kVA$$

TEMPERATURA HLADJENJA PRI OBLI USKUPET JE

$$T_{s1} = R_{th(s-a)} \cdot P_{tot1} + T_a = 0,025 \frac{K}{W} \cdot 2951,3 + (-10^\circ C) = 63,78^\circ C$$

(8)

$$P_{tot2}^{(1)} = \frac{P_{tot2}}{6} = \frac{1721,6W}{6} = 286,93W$$

$$P_{tot2}^{(1)} = V_{T0} \cdot \frac{I_{m2}}{\pi} + r_d \frac{I_{m2}^2}{4}$$

$$I_{m2} = -\frac{2V_{T0}}{\pi r_d} \pm \sqrt{\frac{4V_{T0}^2}{(\pi r_d)^2} + \frac{4P_{tot2}^{(1)}}{r_d}}$$

$$\frac{4P_{tot2}^{(1)}}{r_d} = \frac{4 \cdot 286,93}{0,45} \cdot 10^3 = 2550488,89$$

$$I_{m2} = -1273,88 + \sqrt{1622783,88 + 2550488,89}$$

$$I_{m2} = 768,98A \Rightarrow I_{eff2} = \frac{I_{m2}}{\sqrt{2}} = 545,375A$$

$$S_{opt2} = 3 \cdot \frac{400V}{\sqrt{3}} \cdot 545,375A = 378,3kVA$$

Temp. tranzistora pri ovim uslovima je:

$$T_{s2} = R_{th(s-a)} \cdot P_{tot2} + T_{a2} = 0,025 \frac{K}{W} \cdot 1721,6W + 40^\circ C$$

$$T_{s2} = 83,04^\circ C$$

rezime:

za prvu temp. okoline od  $-10^\circ C$  do  $+40^\circ C$

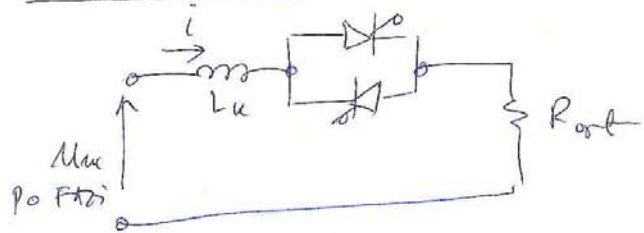
opt. prava snaga (pri ovim) je od 378,3kVA (pri  $+40^\circ C$ ) do

577,83kVA (pri  $-10^\circ C$ ).

Temperatura tranzistora se pri ovim uslovima mora u opt. cu

$$63,78^\circ C \leq T_s \leq 83,04^\circ C$$

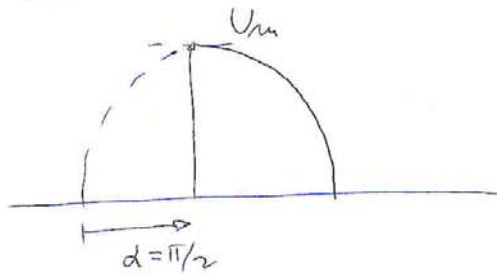
PROJEKCIJA  $L_k$  :



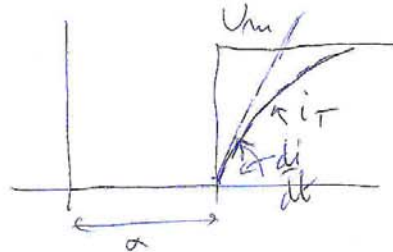
uvjetovanje za snagu

$$U_{max} \text{ i } I_{max} = I_{avg} = 1174,6 \text{ A}$$

zato se mora  $\frac{di}{dt}$  veći



=>



$$i_r = \frac{U_m}{R_{opt}} \left(1 - e^{-\frac{t}{\tau}}\right) \quad \tau = \frac{L_k}{R_{opt}}$$

$$\frac{di_r}{dt} \leq \left(\frac{di_r}{dt}\right)_{ve} = 250 \text{ A}/\mu\text{s} \quad (\text{iz uslova niza, tabela 1})$$

$$\frac{di_r}{dt} = -\frac{U_m}{R_{opt}} \left(-\frac{1}{\tau}\right) e^{-\frac{t}{\tau}} = \frac{U_m}{R_{opt} \cdot \frac{L_k}{R_{opt}}} e^{-\frac{t}{\tau}} = \frac{U_m}{L_k} e^{-\frac{t}{\tau}}$$

$$\frac{di_r}{dt} \Big|_{t=0} = \frac{U_m}{L_k} \leq 250 \frac{\text{A}}{\mu\text{s}} \Rightarrow L_k \geq \frac{U_m}{250 \frac{\text{A}}{\mu\text{s}}}$$

$$U_m = \frac{400}{\sqrt{3}} \text{ (po Fazi)} \approx 230 \text{ V}$$

$$L_k \geq \frac{\frac{1}{\sqrt{3}} 400 \cdot \sqrt{2} \text{ V}}{250 \frac{\text{A}}{\mu\text{s}}} = 1,3 \mu\text{H}$$

$$\text{u stvari se } L_k^* = 2 \mu\text{H}$$

$$\text{pri ovim uslovima stvarni } \frac{di_r}{dt} = \frac{U_m}{L_k^*} = \frac{230 \sqrt{2} \text{ V}}{2 \mu\text{H}} = 162 \frac{\text{A}}{\mu\text{s}}$$

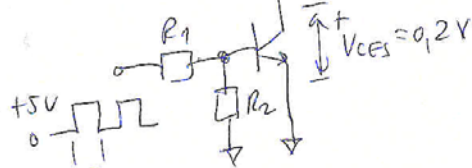
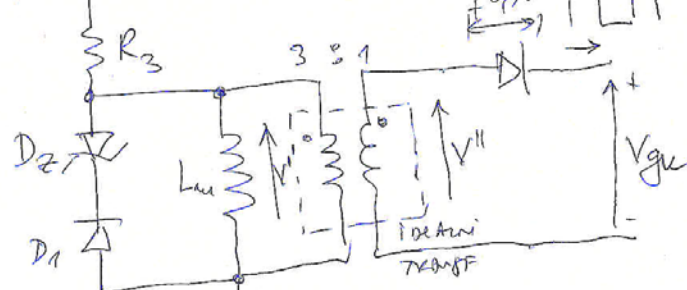
+ To je veće od navedenog 250  $\frac{\text{A}}{\mu\text{s}}$ .

# Dimensioniranje pogona klat:

5

Elektr. del

$+V_{cc} = +24VDC$



$$t_{on} = t_{off} = \frac{1}{2}T = 62,5\mu s \quad R_3 \approx 20\Omega$$

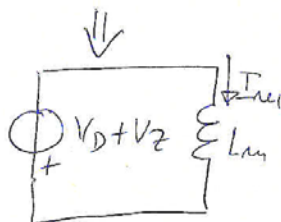
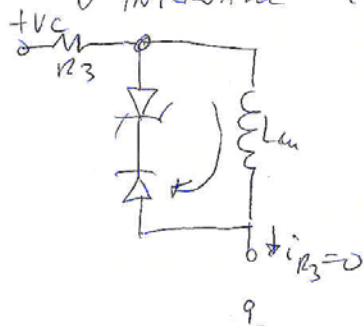
Efektivna vrednost spreze optoka  $R_3$  je  $I_{effR_3} = \frac{I'}{\sqrt{2}} = \frac{0,333A}{\sqrt{2}}$

$$I_{effR_3} = 0,212A$$

$$P_{R_3} = R_3 I_{effR_3}^2 = 20 \cdot 0,212^2 = 0,905W$$

Možnost za  $R_3 = 20\Omega / 1W$

V intervalu toff se  $L_m$  prazni preko  $D_1 - D_2$  preko



$$L_m \cdot \Delta i = V' \cdot t_{on} \Rightarrow \Delta i = I_m = \frac{V' \cdot t_{on}}{L_m}$$

$$\Delta i = \frac{17,1 \cdot 62,5\mu s}{50\mu s} = 21,3mA$$

$$I_m = 21,3mA$$

$$i_{Lm} | I_m = 21,3mA$$

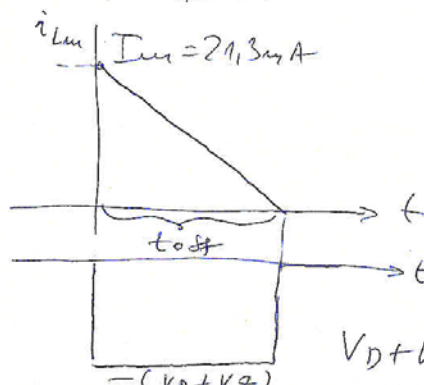
$$-L_m \Delta i = -(V_D + V_Z) \cdot t_{off}$$

$$t_{off} \leq 62,5\mu s$$

$$t_{off} = \frac{L_m \cdot \Delta i}{V_D + V_Z} \leq 62,5\mu s$$

$$V_D + V_Z \geq \frac{L_m \cdot \Delta i}{62,5\mu s}$$

$$V_D + V_Z = \frac{50\mu s \cdot 21,3mA}{60\mu s} = 17,75V$$



⑥

$$V_D + V_Z = 17,75V \quad V_D = 0,7$$

$$V_Z = 17V$$

uzorka Zener dioda 17V i ta struja 21,3mA ( $P_D = 17 \cdot 21 \cdot 10^{-3}$ )  
 $P_D = 0,362W$

\* Uzorko Zener dioda 17V/0,5W

Proračun otpornika  $R_1$  i  $R_2$ .

Uzmemo  $R_2 = 10k\Omega$ .

$$I_{R2} = \frac{V_{BE5}}{R_2} = \frac{0,75V}{10k} = 0,075mA \quad I_{CT} = I' = 0,333A$$

$$I_{BT} = \frac{I_{CT}}{h_{FE}} = \frac{0,333}{300} = 1,11mA$$

$$I_{R1} = I_{BT} + I_{R2} = 1,11mA + 0,075mA = 1,185mA$$

$$V_{CC} = 5V \quad V_{CC} = R_1 I_{R1} + V_{BE5}$$

$$R_1 = \frac{V_{CC} - V_{BE5}}{I_{R1}} = \frac{5 - 0,75}{1,185} \cdot 10^3 = 3,586 \cdot 10^3 \Omega$$

Uzmemo  $R_1 = 3,6k / 0,25W$

$$P_{R1} = 2,28 \cdot 10^3 \cdot (1,185 \cdot 10^{-3})^2 = 0,00504 \leq 0,25W$$

$$R_1 = 3k6 / 0,25W$$

$$R_2 = 10k / 0,25W$$

Sumarno:

$$R_3 = 20\Omega / 1W$$

$$V_Z = 17V$$

$$R_2 = 10k / 0,25W$$

$$DZ: 17V / 0,5W$$

$$R_1 = 3k6 / 0,25W$$